

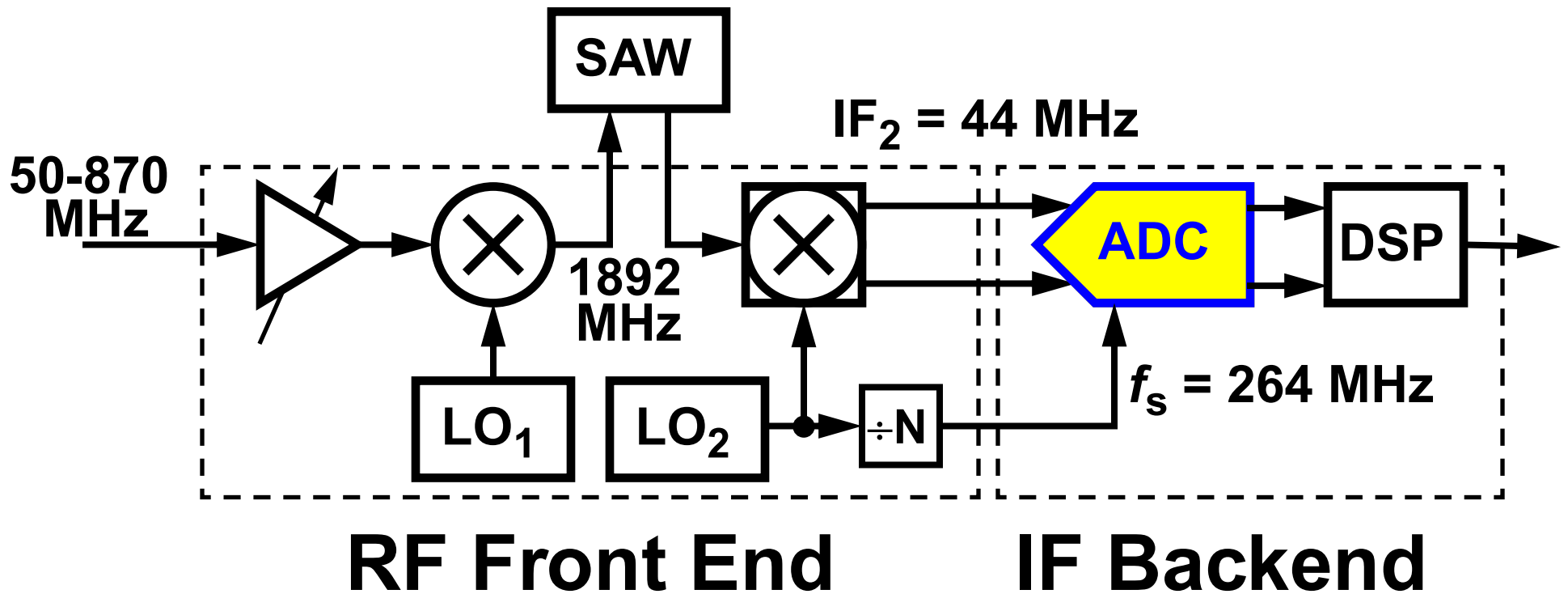
# **A Quadrature Bandpass $\Delta\Sigma$ ADC for a Multi-Standard TV Tuner**

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Cider Seminar  
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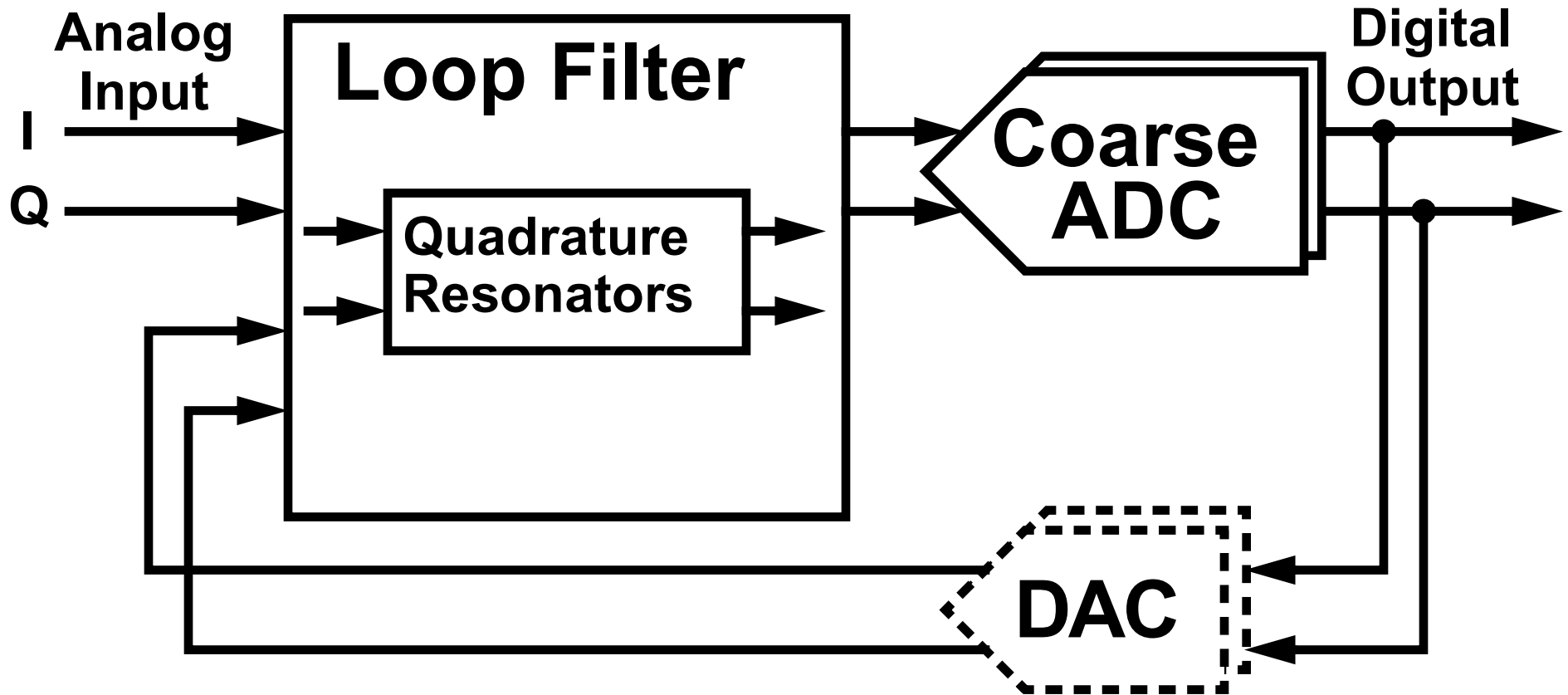
# TV Tuner System



- Dual-conversion super-heterodyne receiver with an ADC at second IF
- ADC input is current-mode I&Q at 44 MHz  
BW = 8.5 MHz

# A Quadrature $\Delta\Sigma$ ADC Is:

[Jantzi 1997]



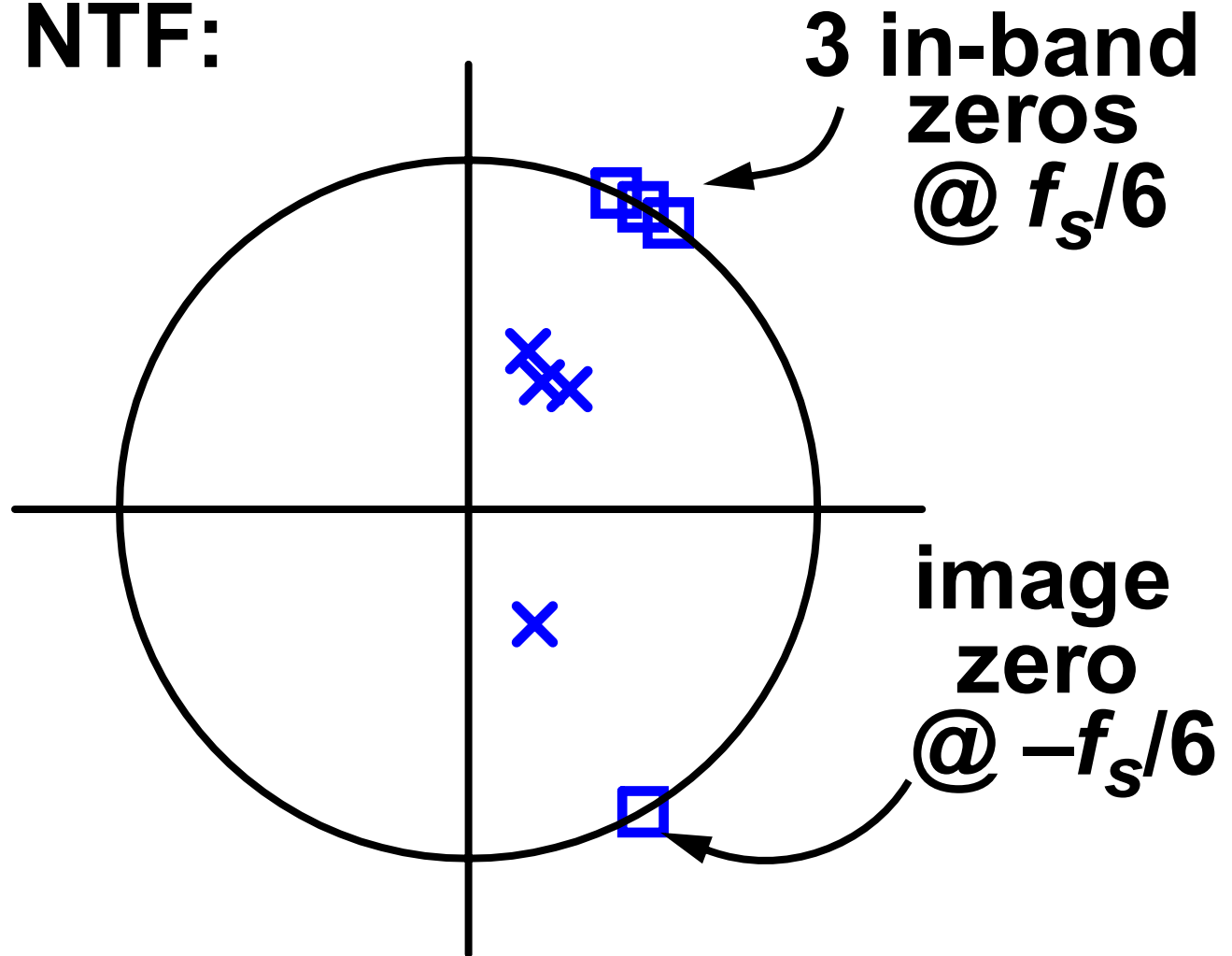
- A  $\Delta\Sigma$  ADC with quadrature everything  
NTF and STF are complex

# Worry List

- 1 DAC linearity and noise at high  $f_s$**   
**⇒ Current-mode DAC, mismatch-shaping**
- 2 Resonator Accuracy:  $f_0$  and Q**  
**⇒ Coming soon!**
- 3 Path Matching**  
**⇒ Large devices, symmetric/merged layout**

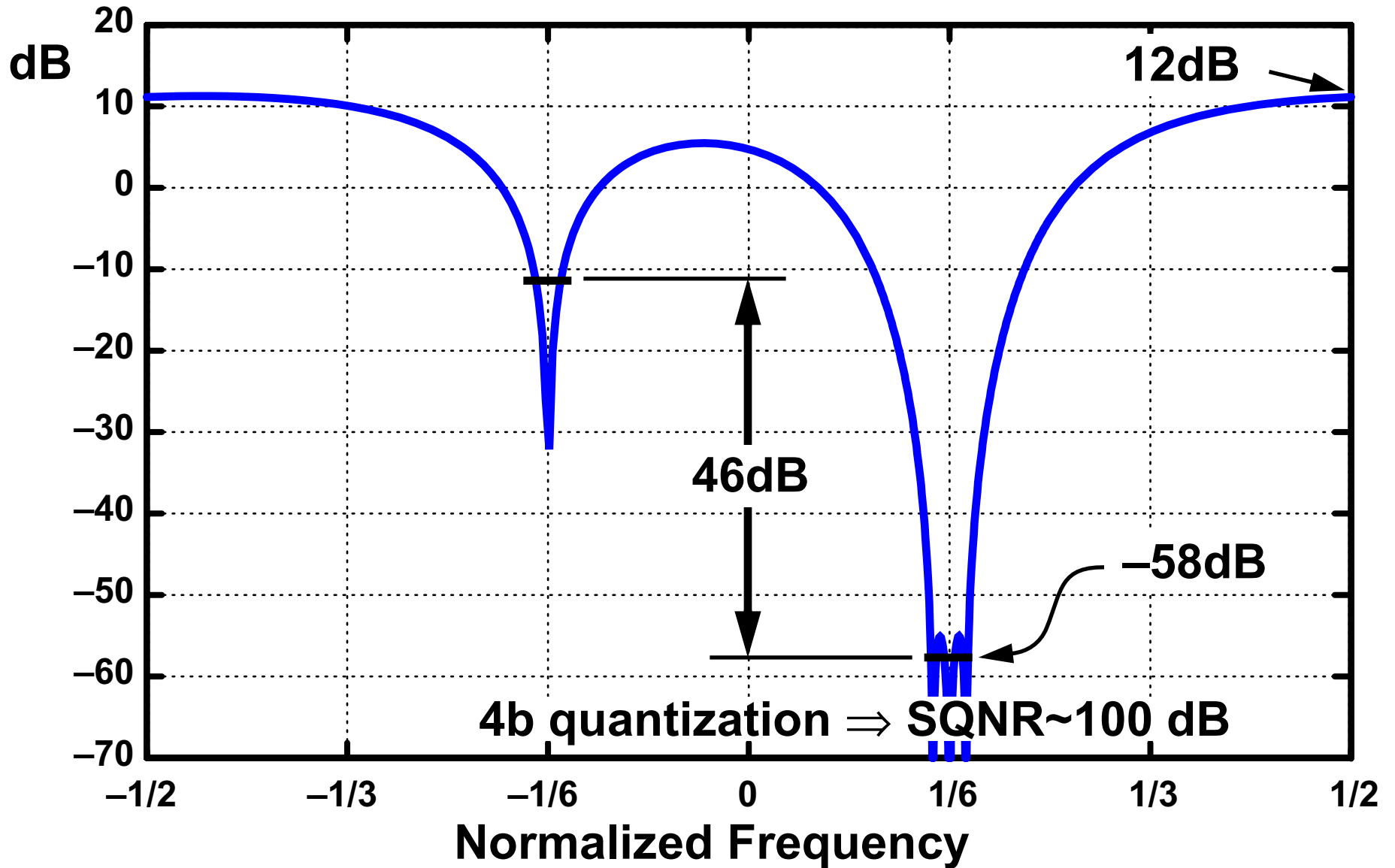
# Ideal NTF– Poles and Zeros

4<sup>th</sup>-order NTF:

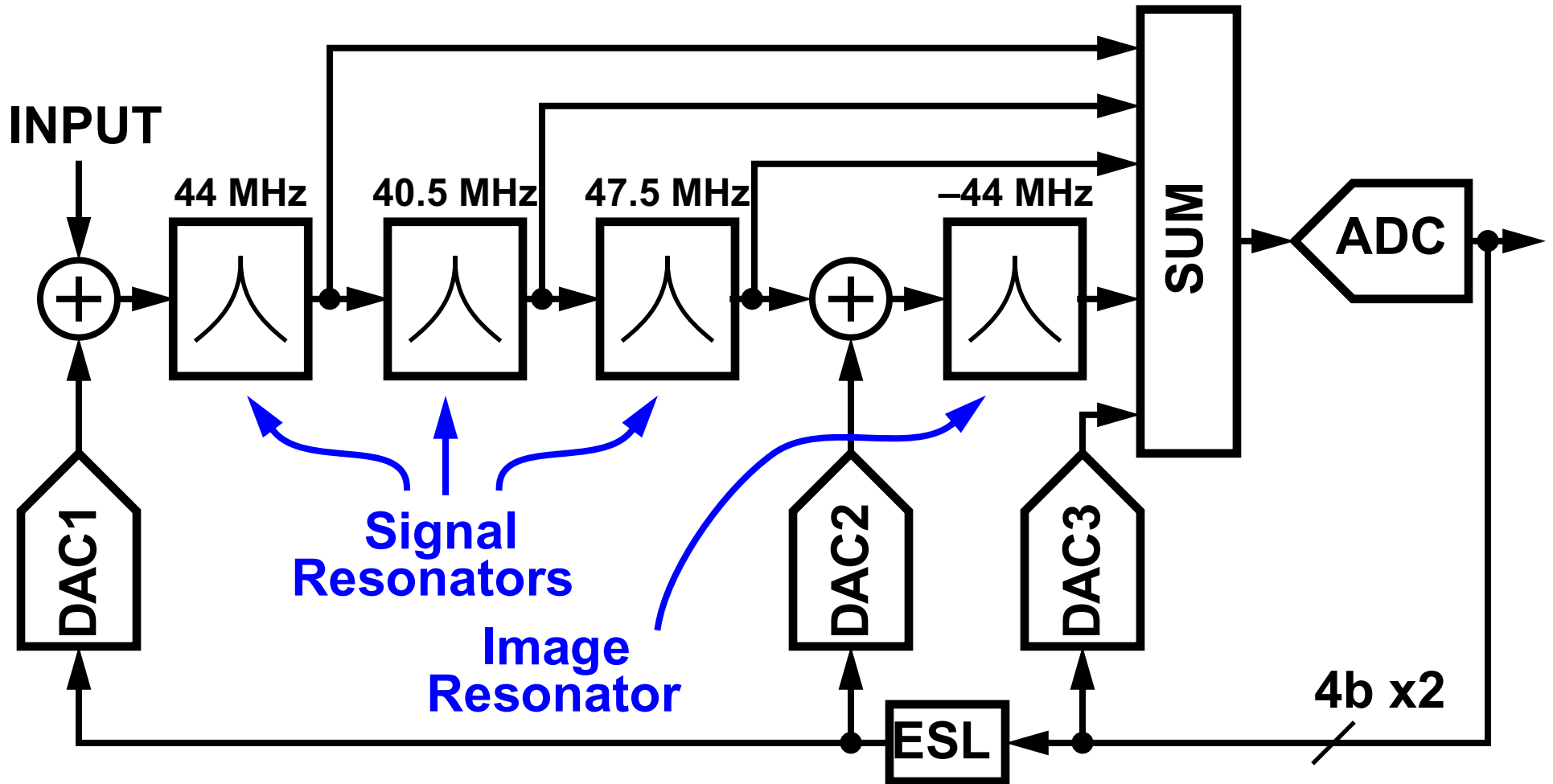


$$\text{OSR} = f_s/f_B = 31$$

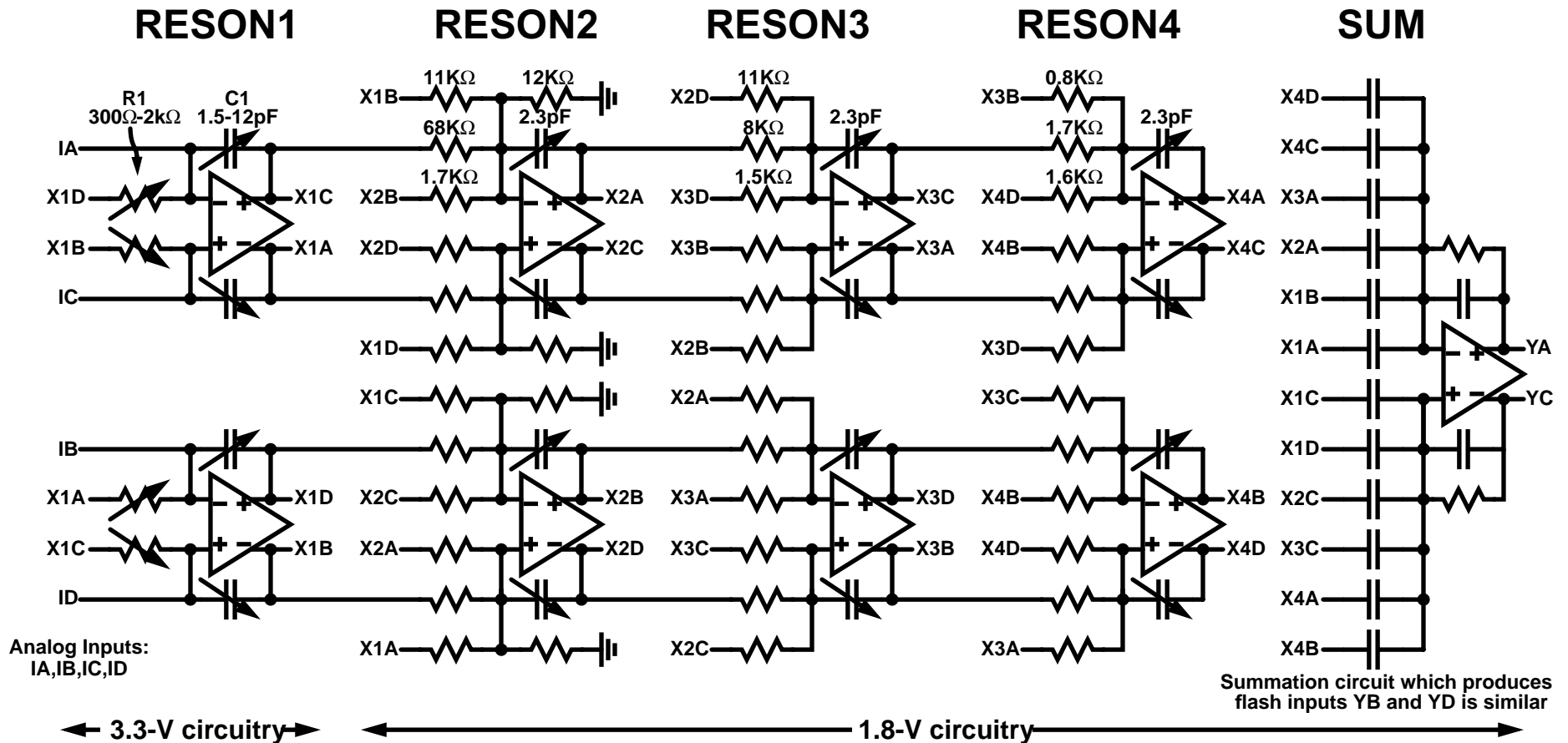
# NTF Magnitude



# ADC Architecture

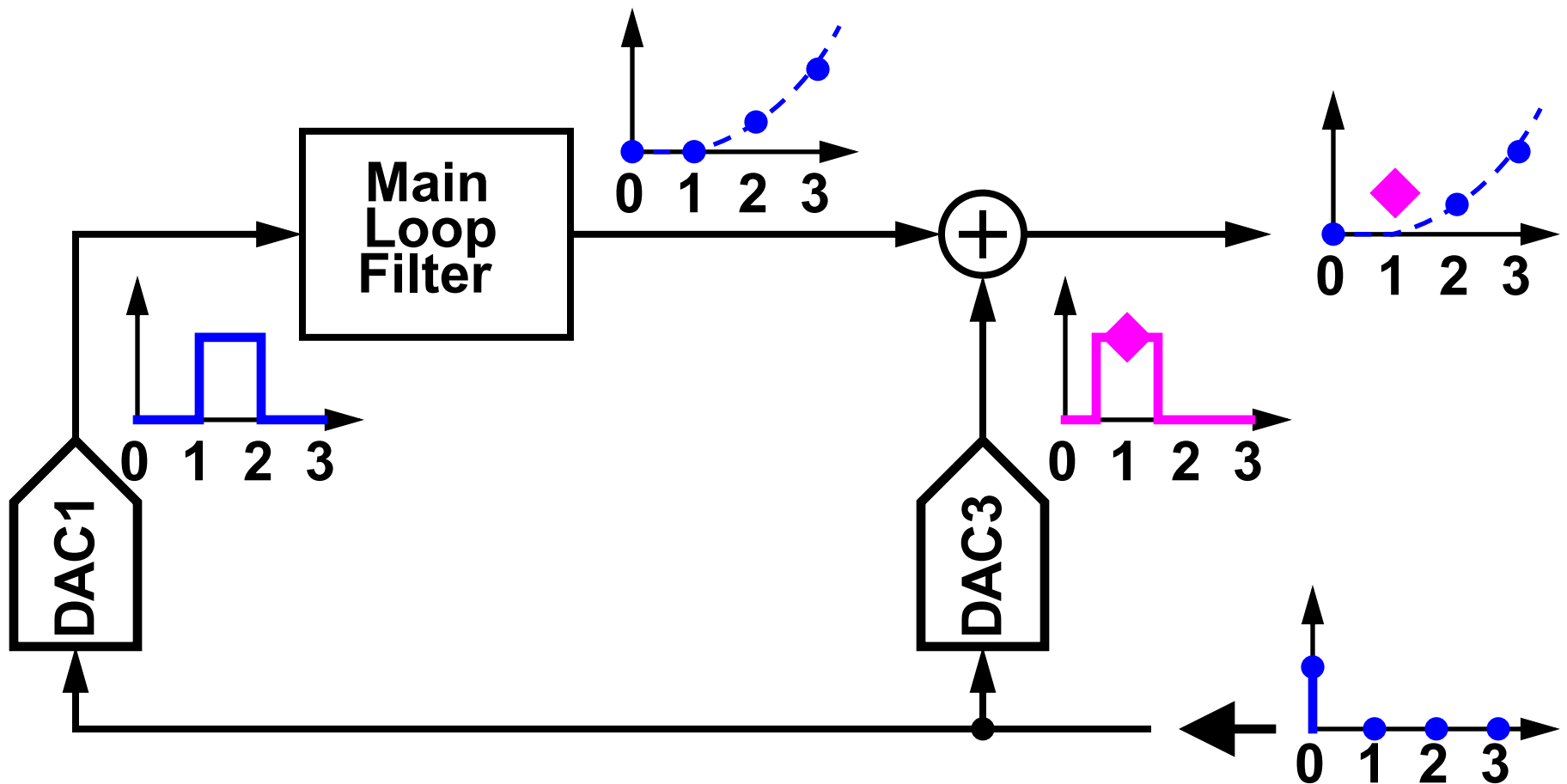


# Loop Filter Schematic

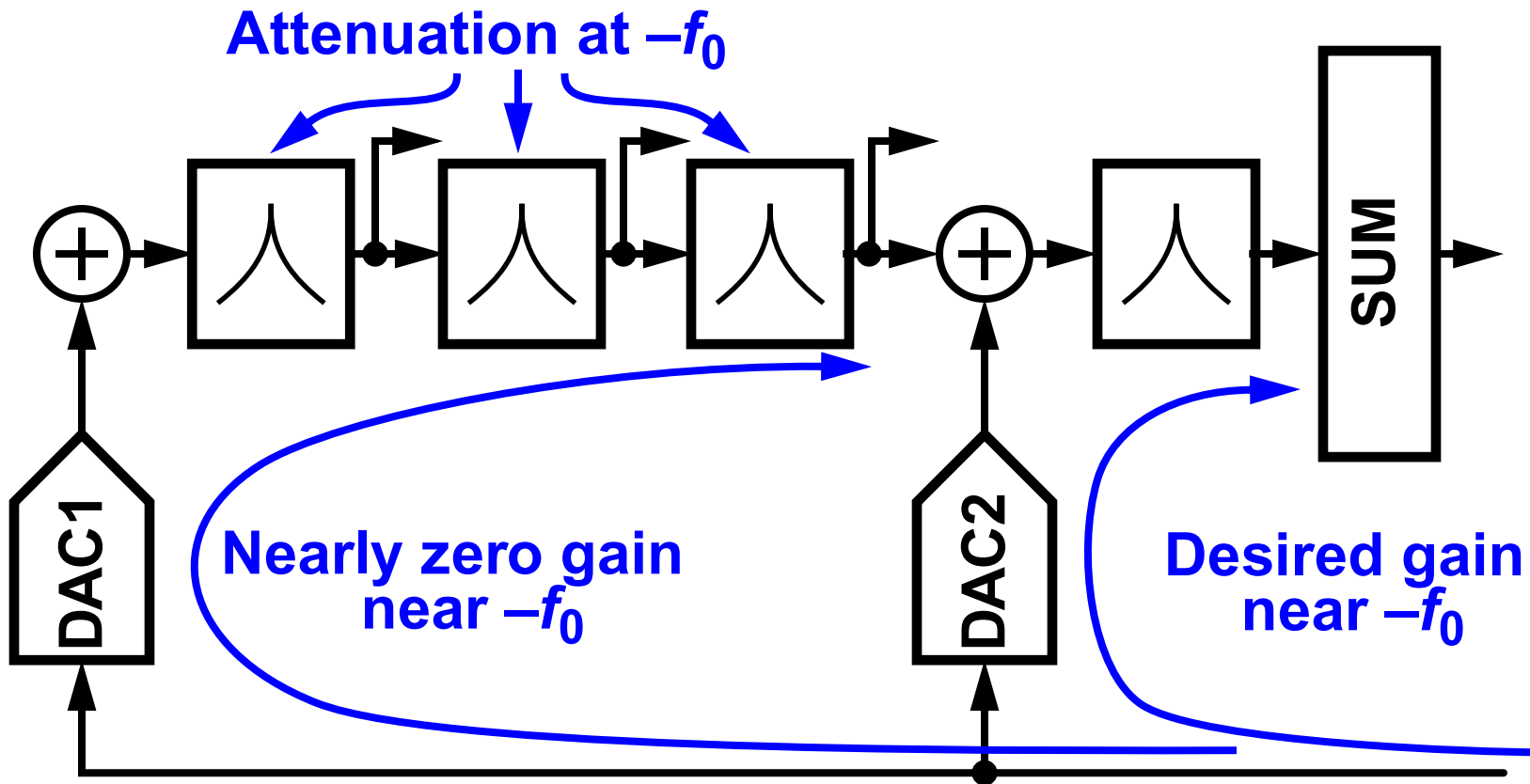


# Why DAC3?

- **DAC3 allows any LF/NTF to be realized**  
Even though DAC1 has 1 clock cycle of delay  
DAC3 supplies the missing point

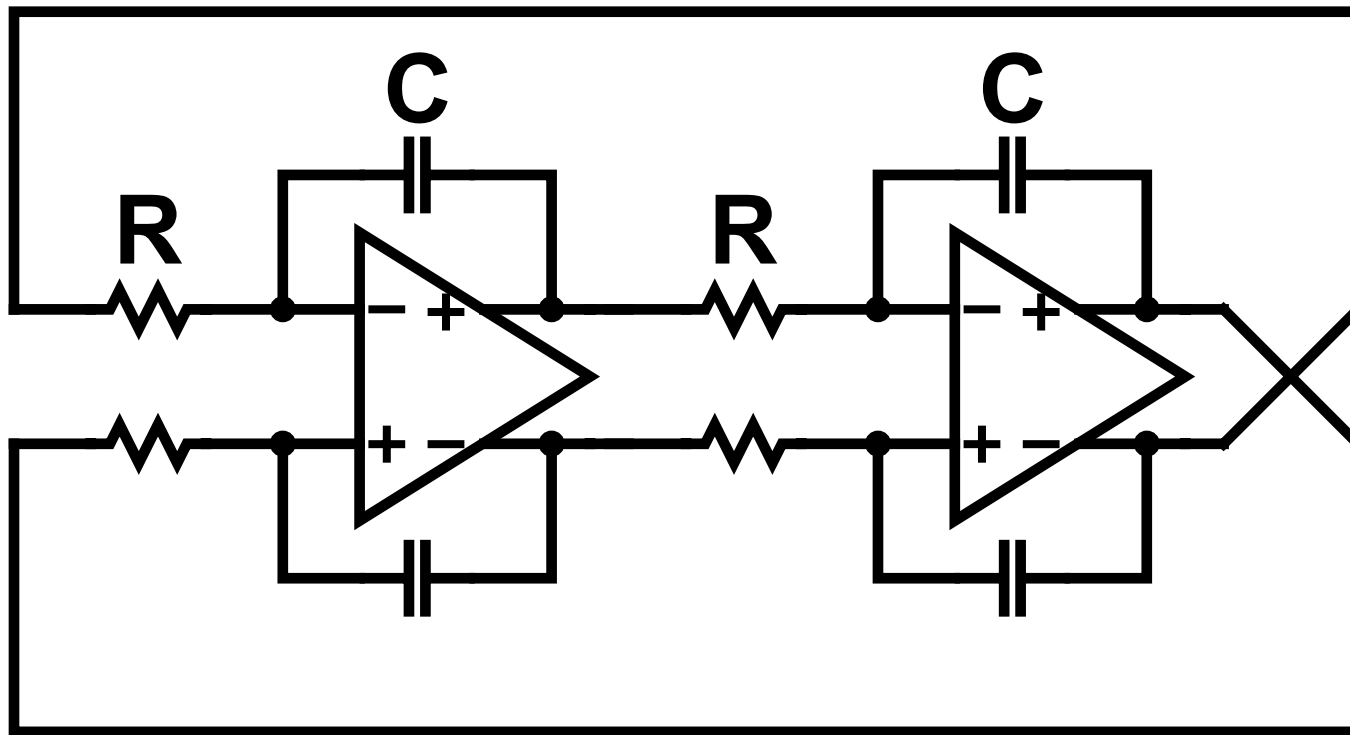


# Why DAC2?



- **DAC2 provides a low-attenuation feedback path for signals in the vicinity of  $-f_0$  thereby resolving a near singularity in the coefficient calculation procedure**

# Resonator Structure

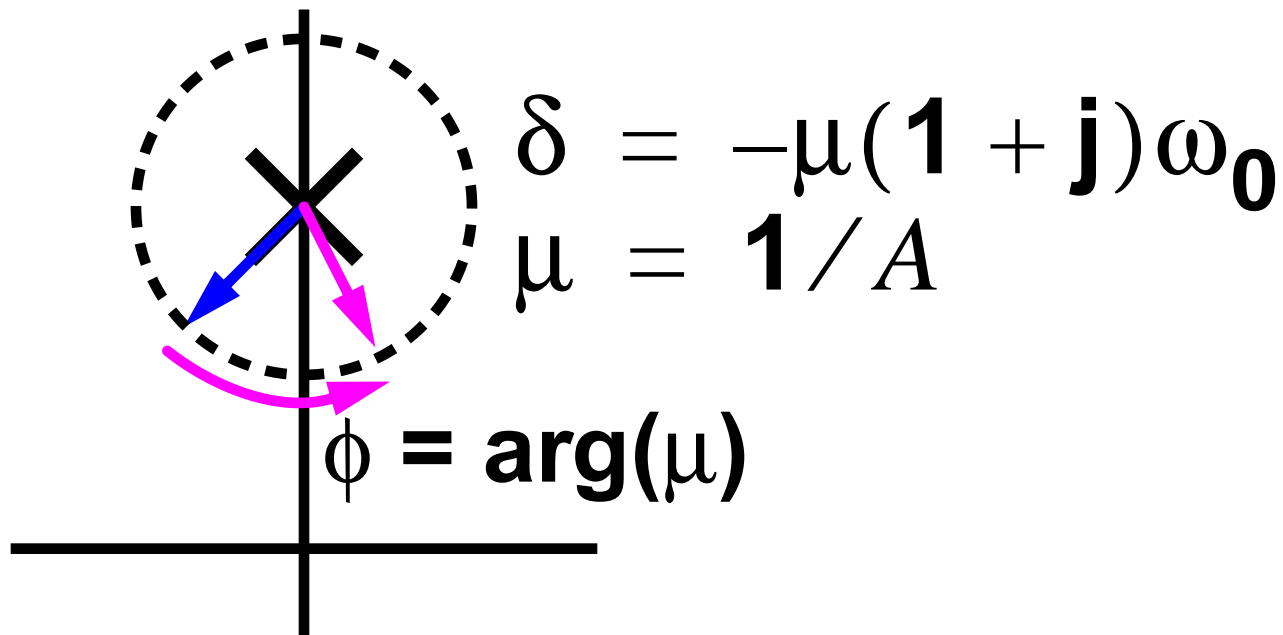


$$f_0 = \frac{1}{2\pi RC}$$

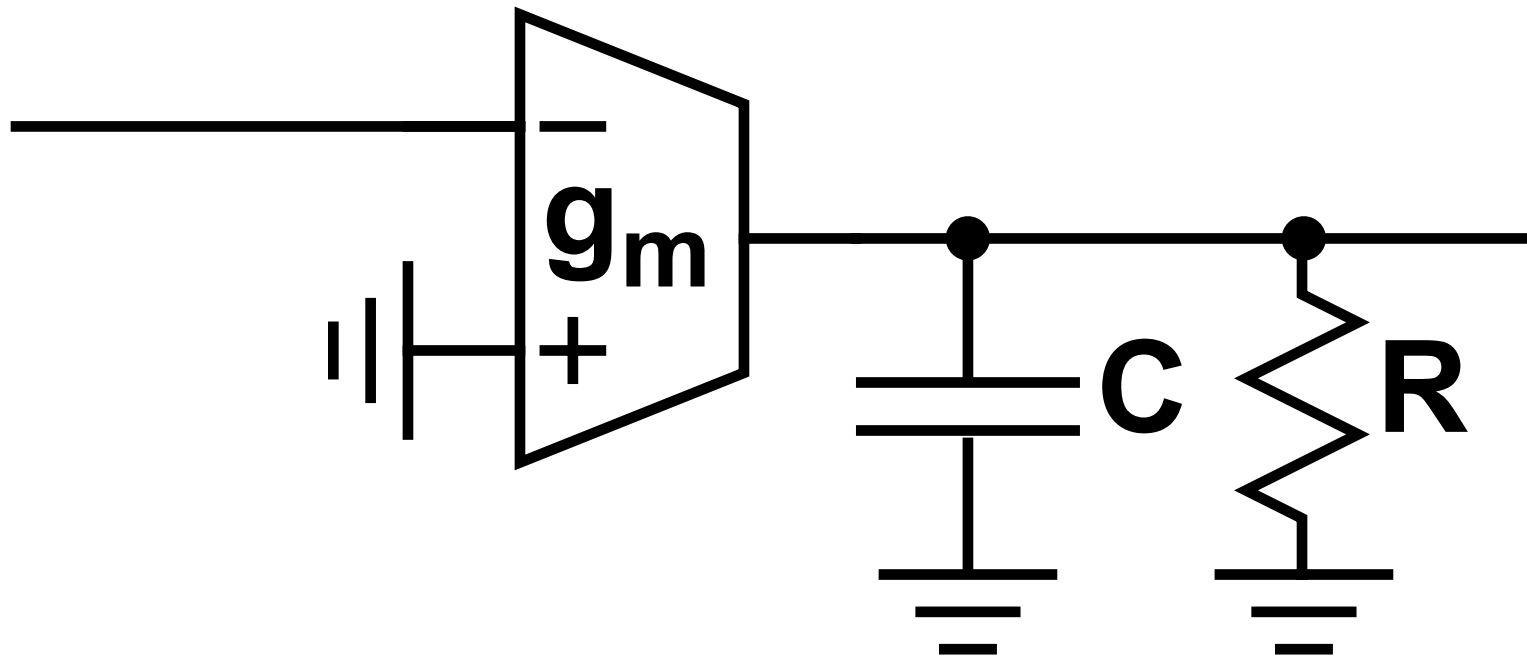
- Tuned by adding positive feedback to make an oscillator and adjusting C until the desired resonance is achieved
- Amplifier drives both R and C  $\Rightarrow$  trouble?

# Amplifier Gain and Phase

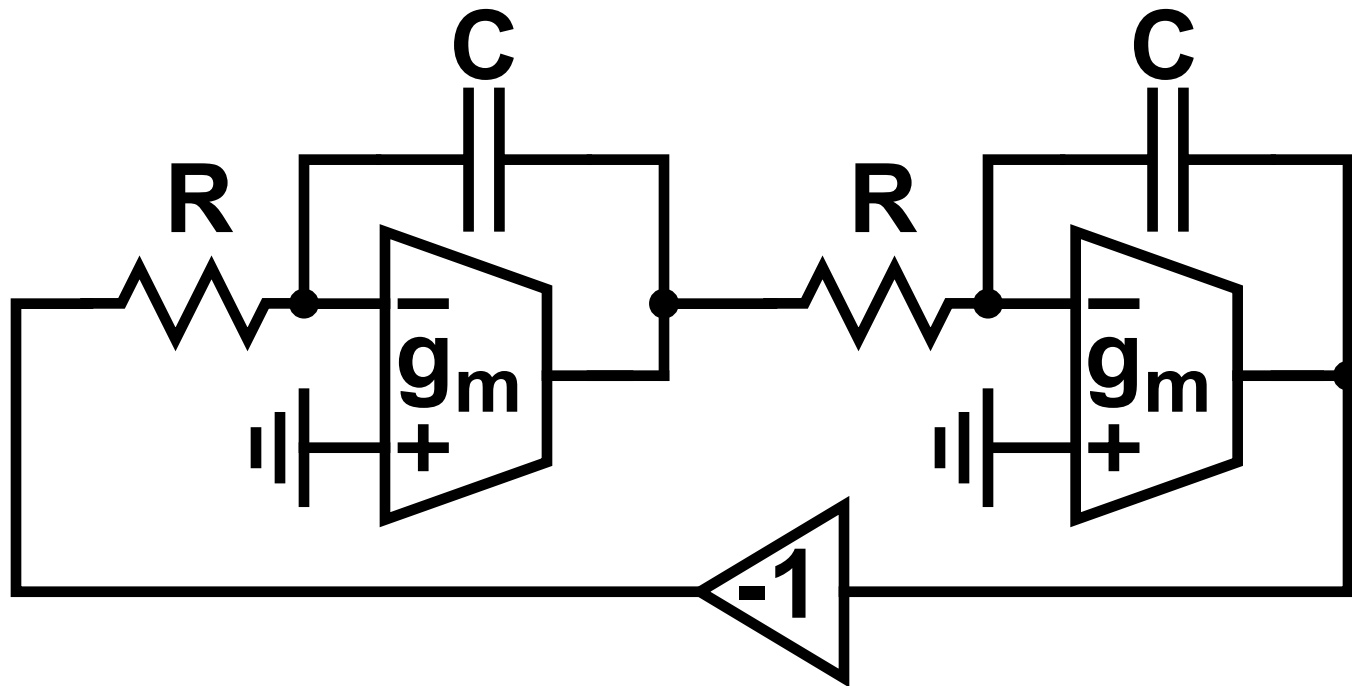
- Finite gain degrades Q
- Phase lag enhances Q
- Analysis shows  $\phi = 45^\circ$  yields high Q, regardless of amplifier gain



# An Amplifier with $\phi = 45^\circ$ @ $f_0$ :



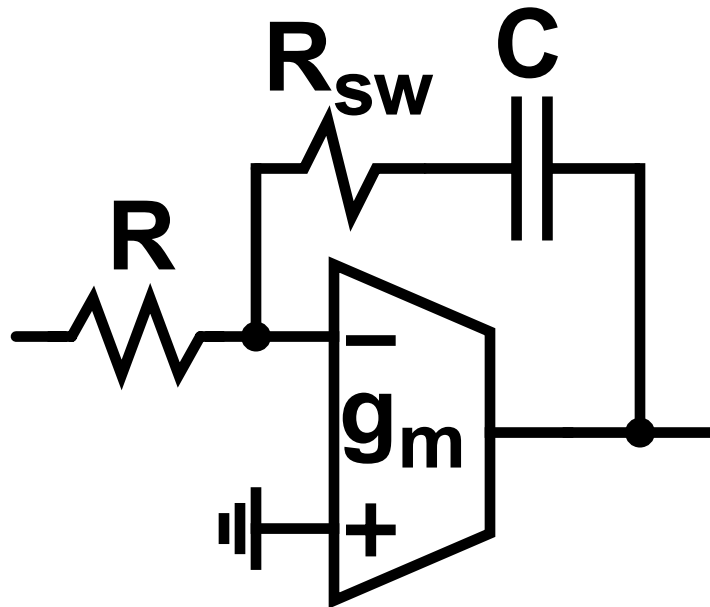
# Resulting High-Q Resonator



- Amplifier load yields  $\phi = 45^\circ @ f_0$
- Finite  $g_m$  shifts the pole frequency, but does not degrade  $Q$ !

# Finite $g_m$ Bandwidth & Non-Zero Switch Resistance

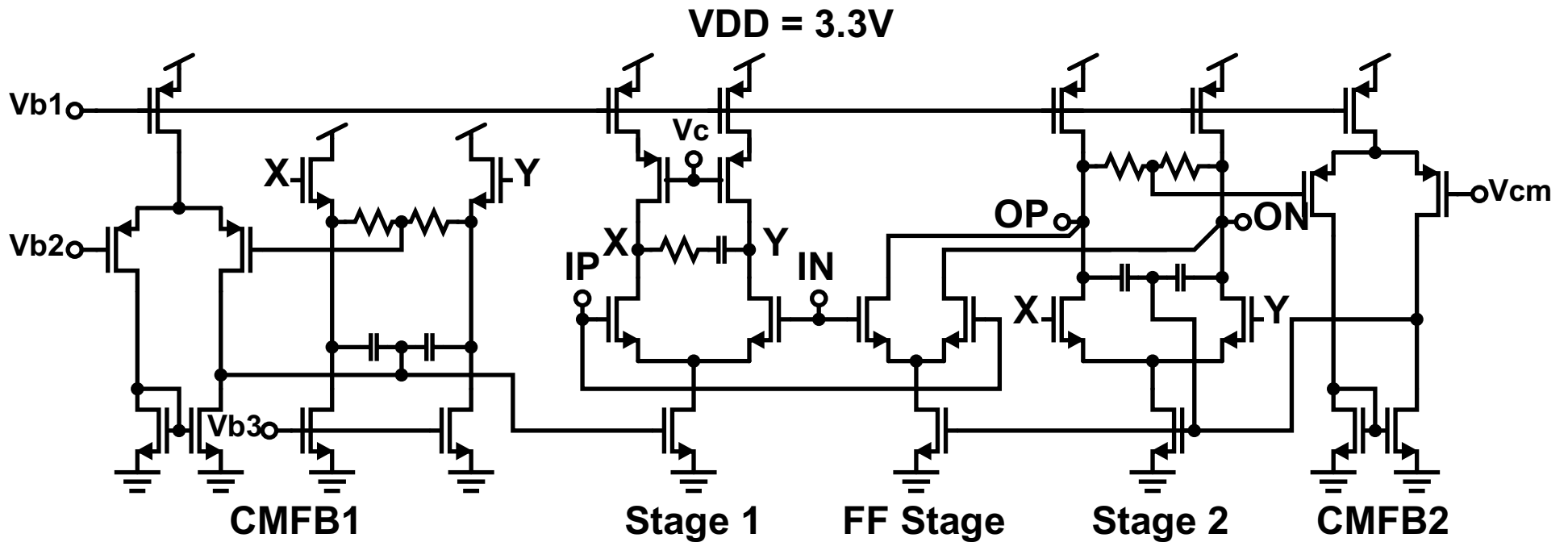
- Switch resistance degrades Q
- Finite gm bandwidth enhances Q



$$g_m = \frac{g_{m0}}{1 + s/\omega_p}$$

- Cancellation occurs if  $R_{sw} = \frac{2\omega_0}{g_{m0}\omega_p}$

# 1<sup>st</sup> Resonator's Amplifier

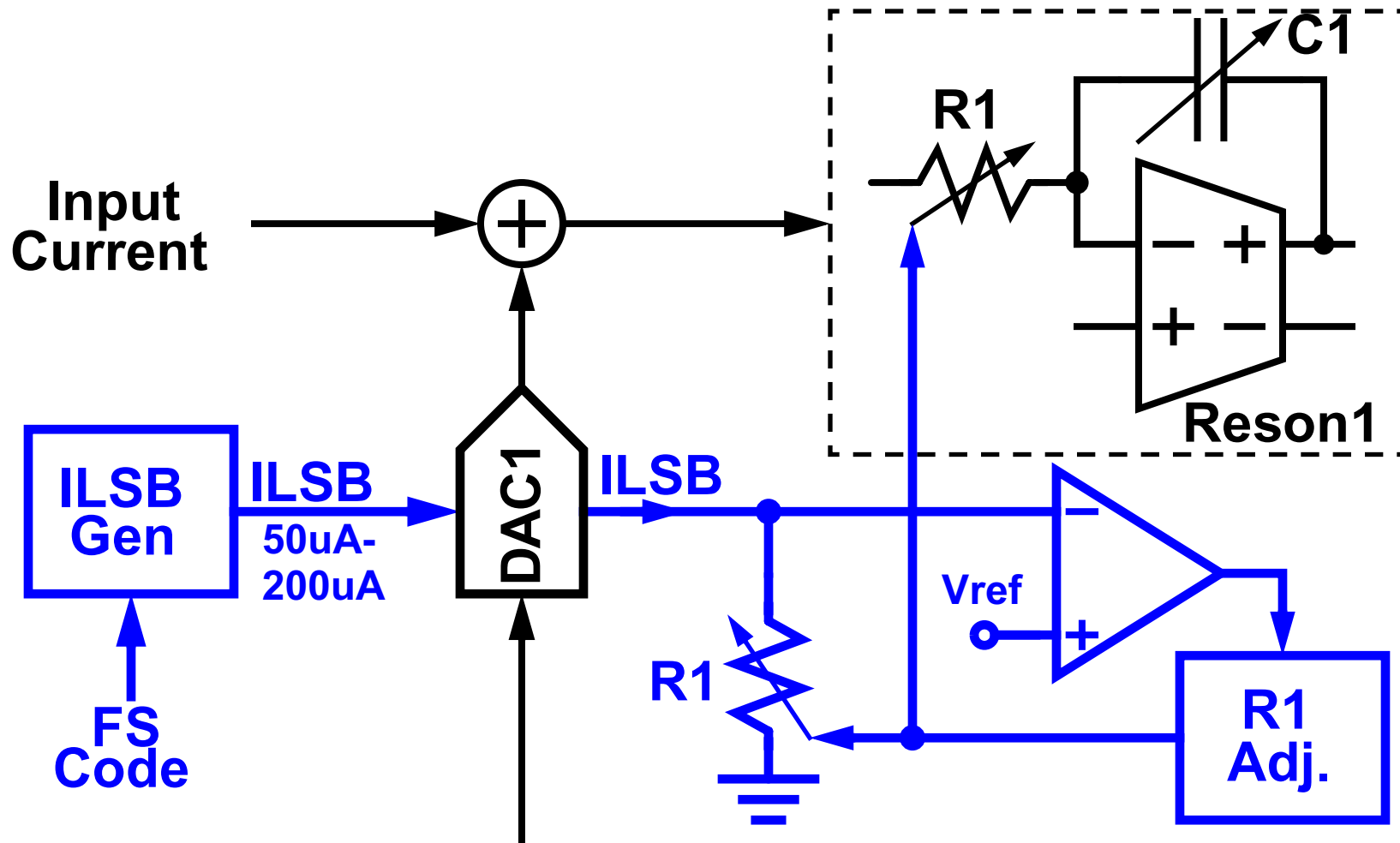


- **2-stage amplifier with feedforward stage and all-NMOS signal path**

# Gain-Scaling

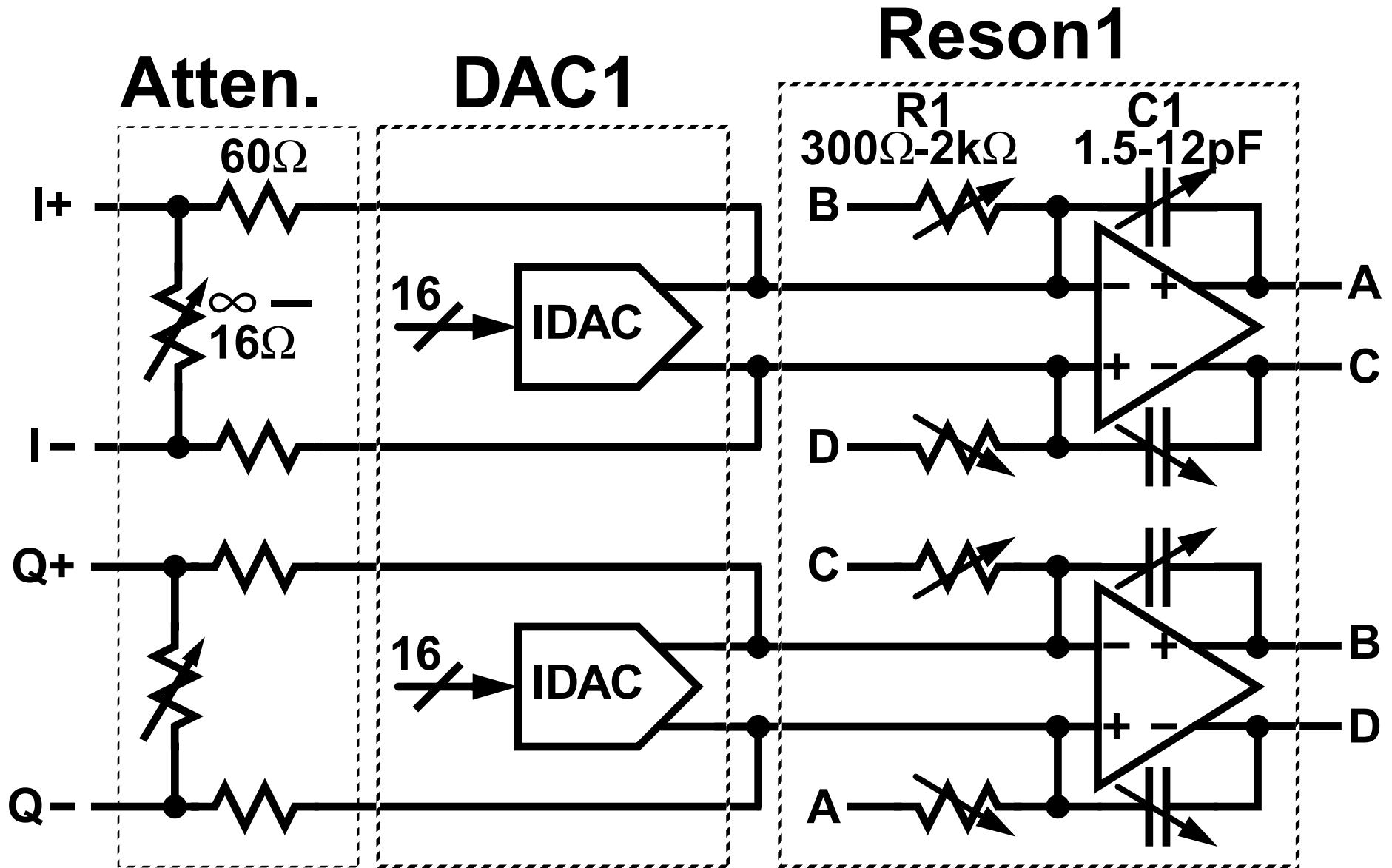
- **12-dB gain range implemented by scaling DAC1's LSB over a 4:1 range**
- **At the minimum LSB setting, DAC1's noise is 6 dB lower than at the maximum LSB setting**
- **Changes in DAC gain are counteracted by inverse change in Reson1 gain**  
**Keeps gain of DAC1-Reson1 independent of LSB setting**
- **The gain-scaling burden is on the front end**  
**No other circuits need to be adjusted**

# Gain-Scaling Arrangement

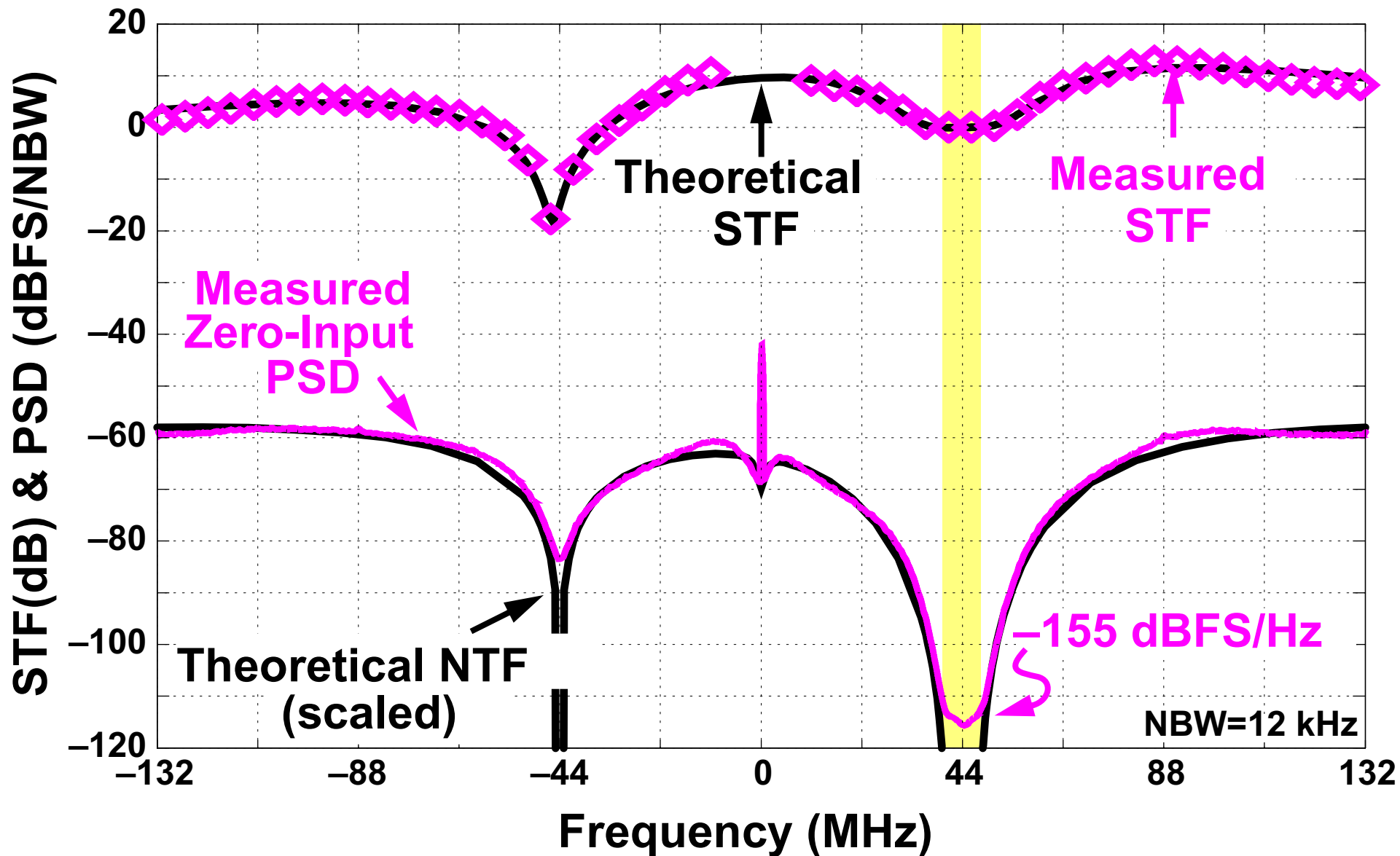


- **Gain of DAC1+Reson1 kept constant**

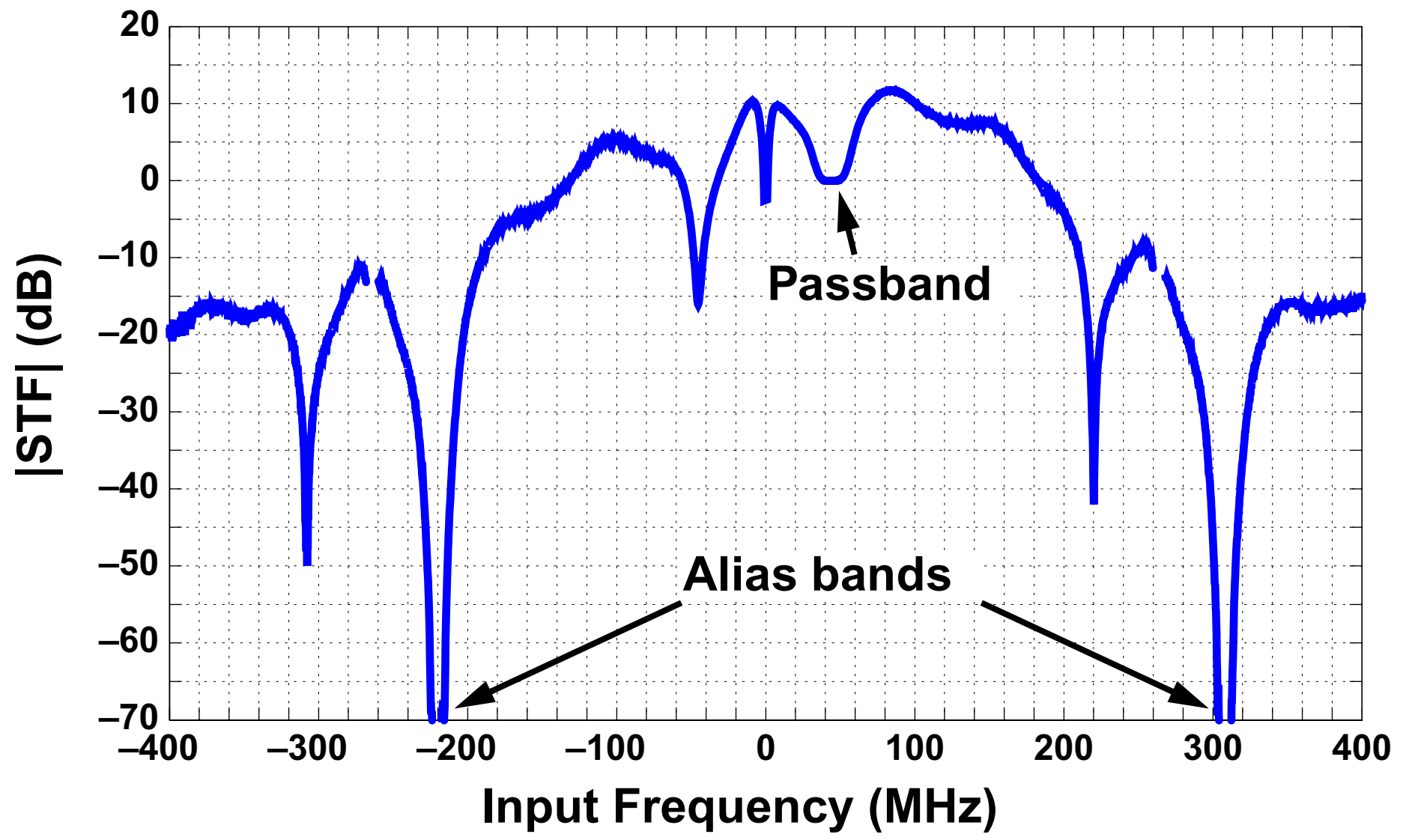
# ADC Front-End



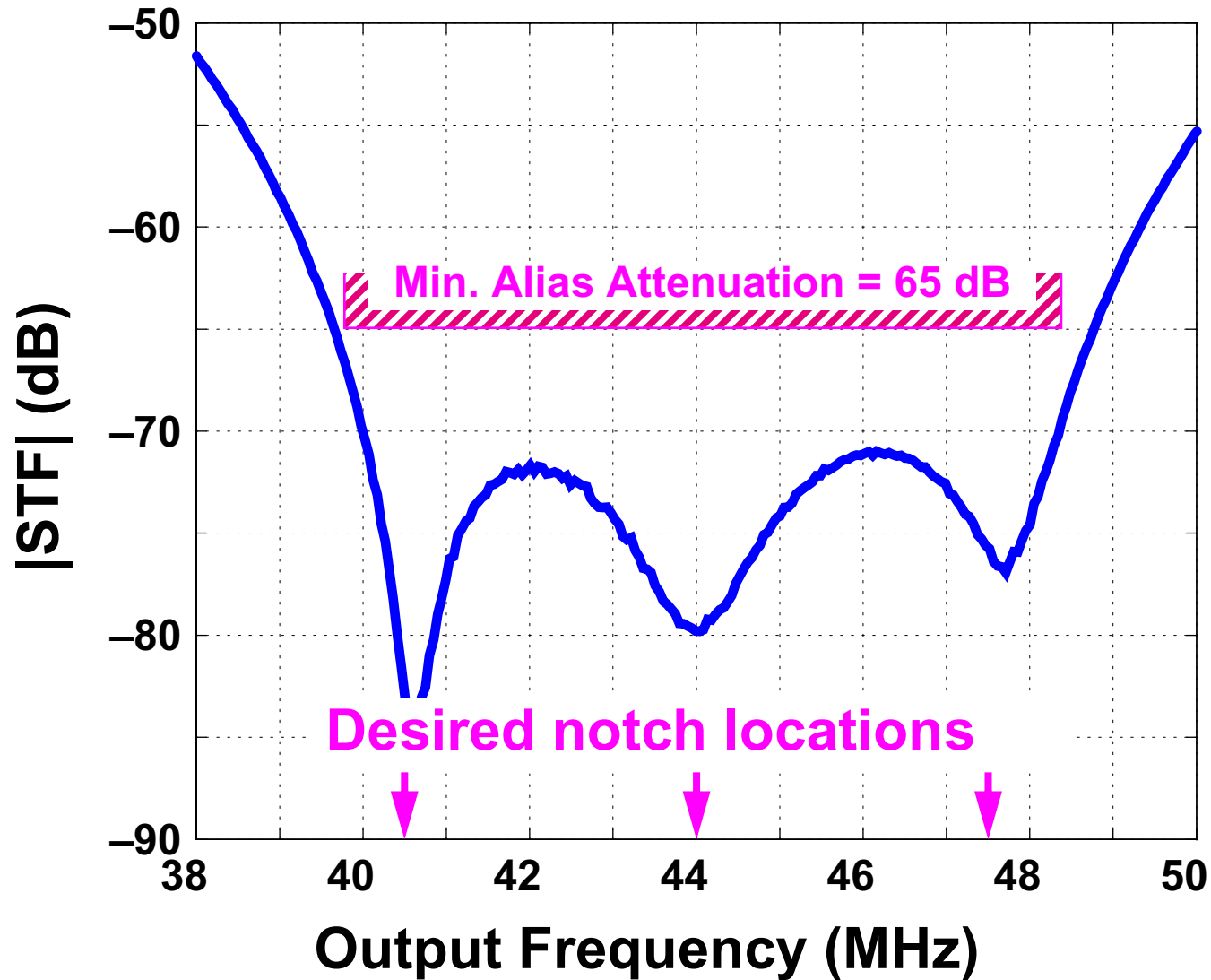
# Results: STF & NTF



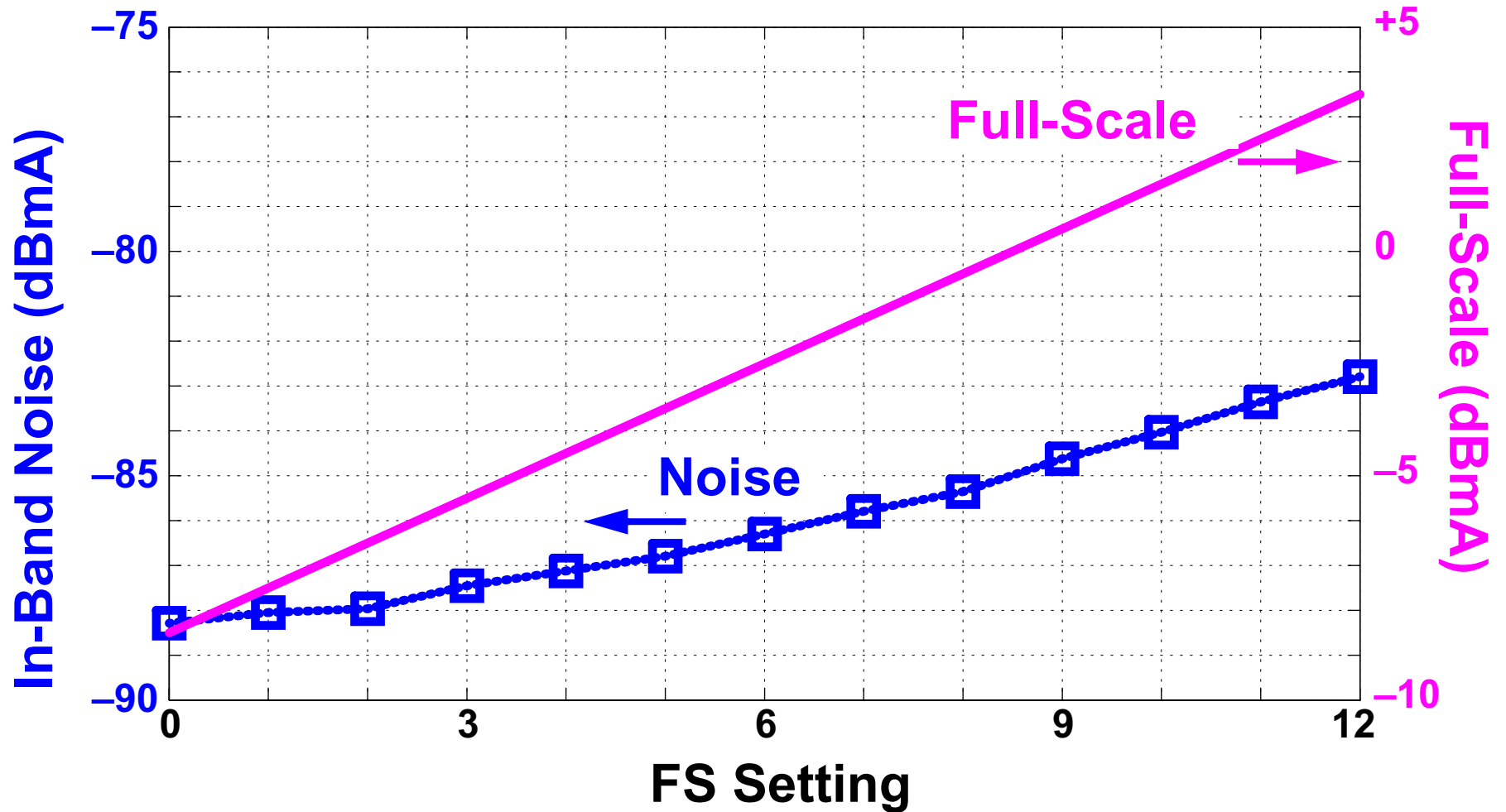
# Wideband STF



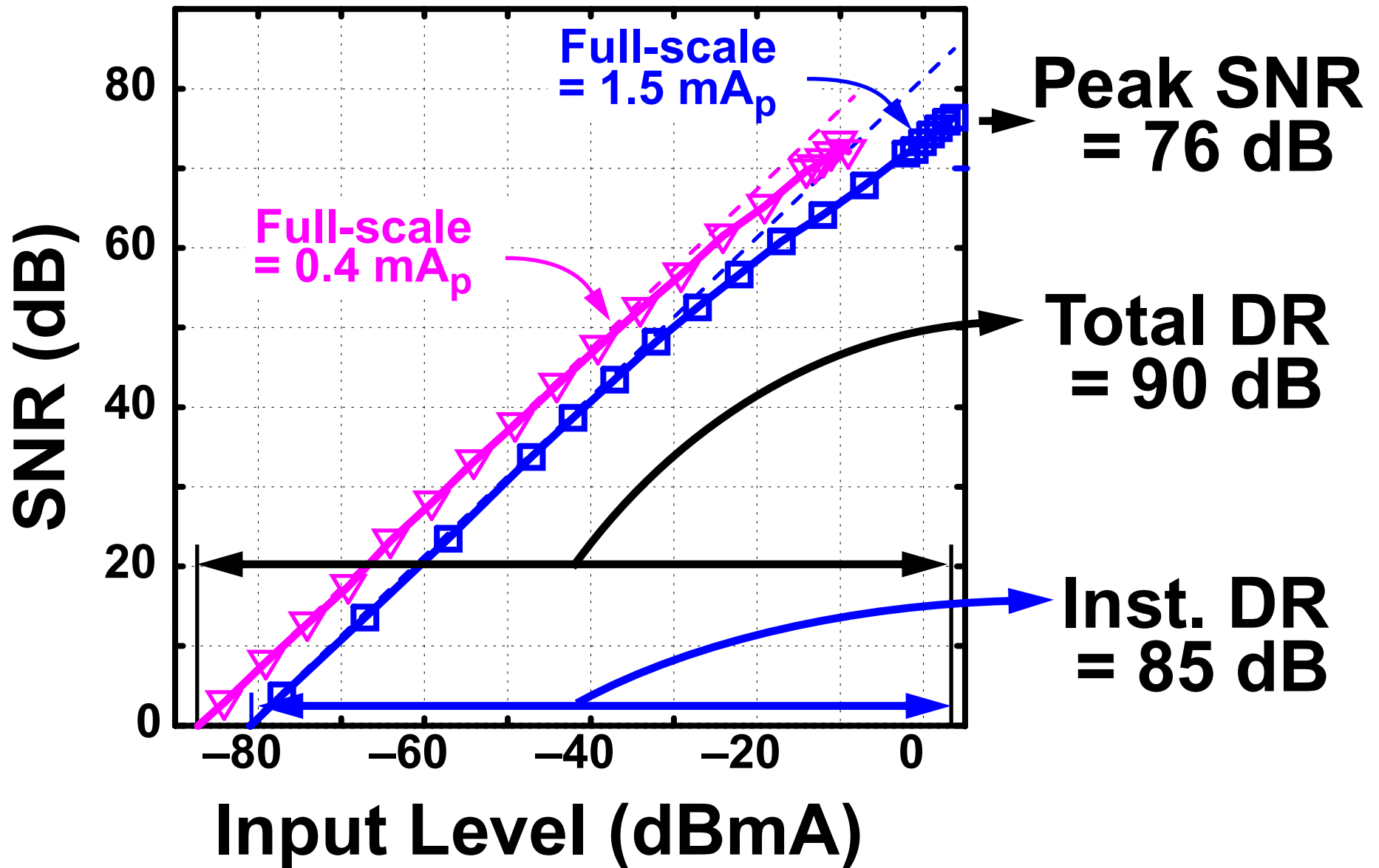
# STF in +1 Alias Band



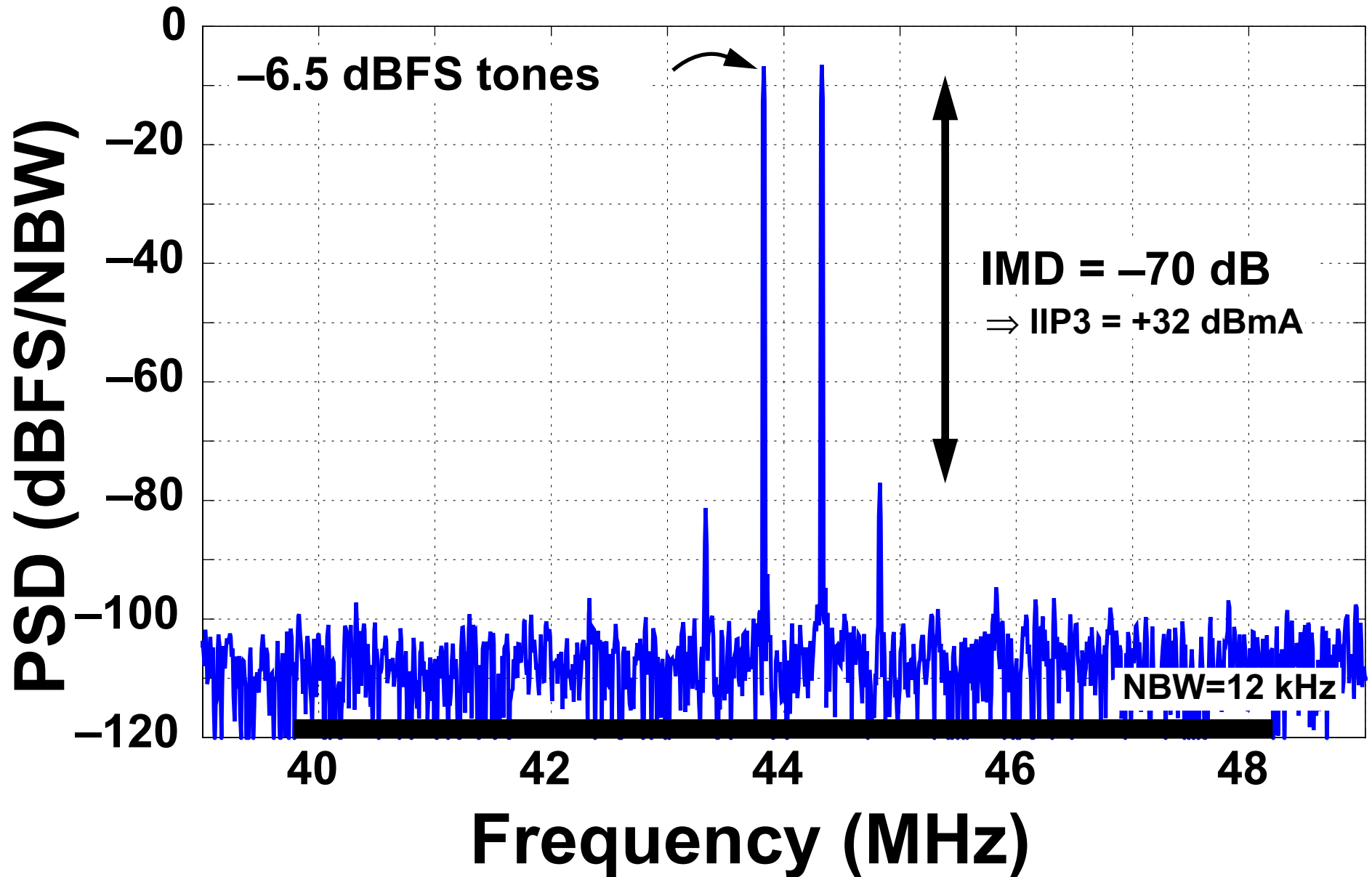
# Noise vs. Full-Scale Setting



# SNR vs. Input Level



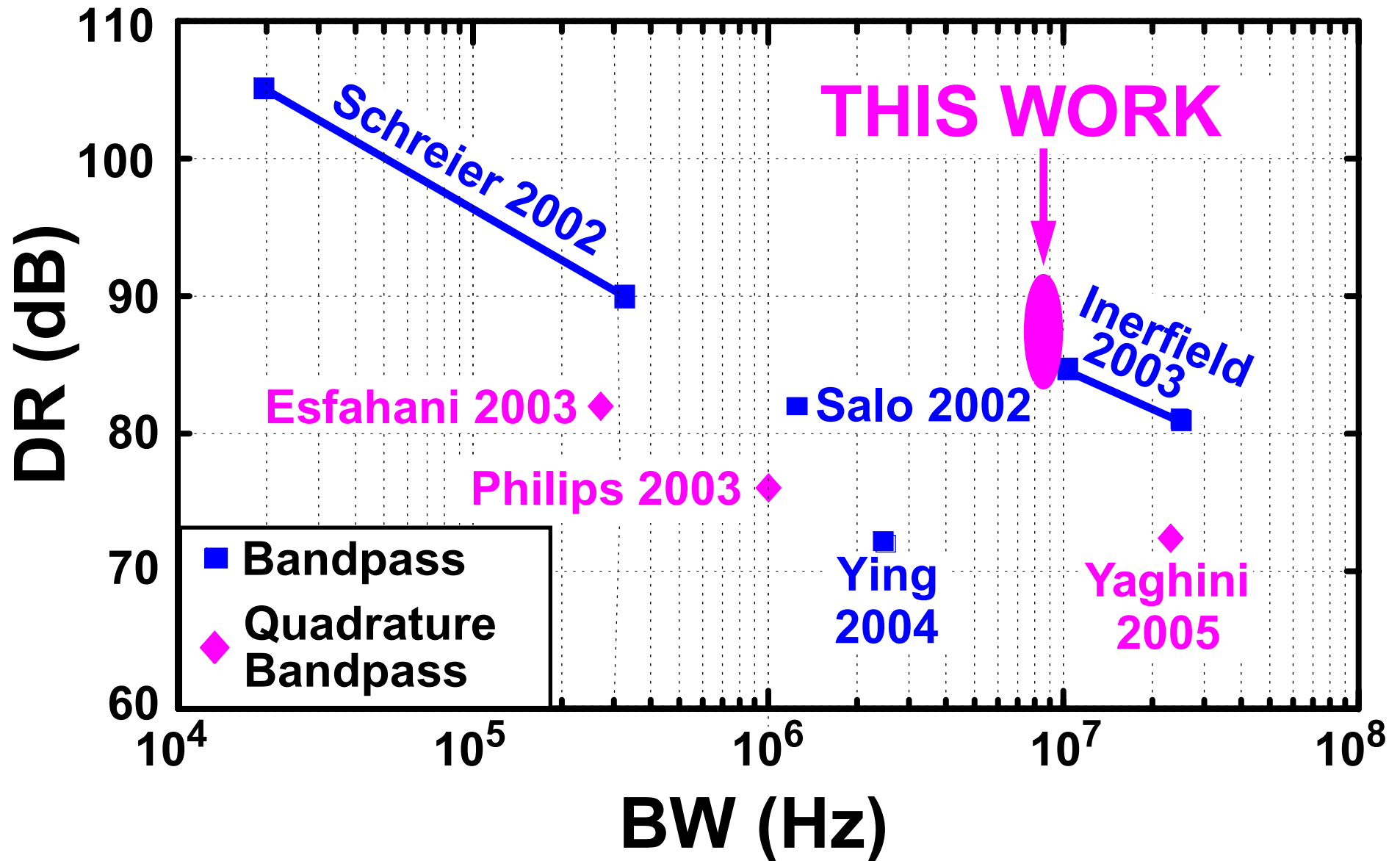
# Two-Tone Spectrum



# Performance Summary

<b>Bandwidth</b>	<b>8.5</b>	<b>MHz</b>
<b>Center Frequency</b>	<b>44</b>	<b>MHz</b>
<b>Clock Frequency</b>	<b>264</b>	<b>MHz</b>
<b>Inst. Dynamic Range</b>	<b>85</b>	<b>dB</b>
<b>Full-Scale Range</b>	<b>12</b>	<b>dB</b>
<b>Total Dynamic Range</b>	<b>90</b>	<b>dB</b>
<b>Area in 0.18um CMOS</b>	<b>2.5</b>	<b>mm<sup>2</sup></b>
<b>Power Consumption</b>	<b>375</b>	<b>mW</b>

# Performance Comparison



# Conclusions



**A feedforward implementation of a Quadrature Bandpass  $\Delta\Sigma$  ADC needs an extra DAC**

**An input attenuator is a good idea too.**



**High Q resonance can be achieved by**

**1. Using a simple  $g_m$  instead of a true op amp**

**2. Balancing finite  $g_m$  bandwidth and non-zero switch resistance**

**Measured  $Q > 40$**



**Gain-scaling extends DR**

