Low Freq Cutoff

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- The low frequency cutoff is generally due to coupling and bypass capacitors
- Coupling and bypass capacitors are intentionally added to the circuit
- Coupling Caps
 - Added in series with the signal so that the dc bias conditions can be different for different parts of the amplifier
 - Or to filter out low freq signals/noise
- Bypass Caps
 - Added across an element (often a current source) so that the element is a high impedance at low freq and a low impedance at high frequencies
 - Makes biasing easier
 - Also filters out low freq signals/noise



- Assume $r_o \rightarrow \infty$
 - Impedance looking into M_1 drain is ∞
 - Impedance looking into M_1 source is $r_s = 1/g_m$
- Include r_{oB} for current source
- Coupling Caps
 - C_{C1} and C_{C2}
- Bypass Cap
 - C_S
 - To bypass current source so v_x looks like ground at midband and high freq
- There are 3 LF (low freq) poles
 - Due to C_{C1} , C_{C2} and C_{S}
- There are 2 zeros at dc, one finite zero
 - dc zeros due to C_{C1} , C_{C2} ; finite zero due to C_S

• 3 LF poles

$$C_{C1} \Rightarrow \omega_{p1} = \frac{1}{C_{C1}(R_i + R_G)}$$
(1)

$$C_{C2} \Rightarrow \omega_{p2} = \frac{1}{C_{C2}(R_D + R_L)}$$
(2)

$$C_S \Rightarrow \omega_{p3} = \frac{1}{C_S(r_s || r_{OB})}$$
(3)

Finite zero due to C_S

$$H(s) = \frac{-(R_D||R_L)}{r_s + (r_{oB}||(1/sC_S))}$$
(4)
$$H(s) = -(R_D||R_L) \times \frac{1 + sC_S r_{oB}}{(r_s + r_{oB}) + sC_S r_s r_{oB}}$$
(5)

 $\omega_{z3} = 1/(C_S r_{oB}) < \omega_{p3}$

Could have found zero by finding where C_S and r_{oB} go to infinite impedance

Example

 $-R_i = 100 \mathrm{k}\Omega; R_G = 4.7 \mathrm{M}\Omega; R_D = 15 \mathrm{k}\Omega; R_L = 15 \mathrm{k}\Omega; r_{oB} \rightarrow \infty$

- $-g_m = 1 \text{mA/V} \Rightarrow r_s = 1/g_m = 1 \text{k}\Omega$
- Select C_{C1} , C_{C2} , and C_S so $f_L \approx 100$ Hz by having 1 pole at 100Hz and 2 poles each at 10Hz. Also, minimize the total capacitance size.
- Solution
 - $-\omega_{p1} = \frac{1}{C_{C1}(R_i + R_G)}$ $\omega_{p2} = \frac{1}{C_{C2}(R_D + R_L)}$ $\omega_{p3} = \frac{1}{C_S r_s}$
 - Since $r_s < (R_D + R_L) < (R_i + R_G)$, to minimize capacitance, make ω_{p3} be the largest pole at 100Hz
 - $C_s = \frac{1}{\omega_{p3}r_s} = \frac{1}{(2\pi \times 100)(1k)} = 1.6\mu F$
 - Now let $\omega_{\rho 1} = \omega_{\rho 2} = 2\pi \times (10 \text{Hz})$
 - $-C_{C1} = \frac{1}{\omega_{p1}(R_i + R_G)} = 3.3 \text{nF}$

$$-C_{C2} = \frac{1}{\omega_{p2}(R_D + R_L)} = 0.53 \mu F$$

- Low freq cutoff
- Due to added coupling or bypass capacitors
 - Added to simplify design or to filter dc signals