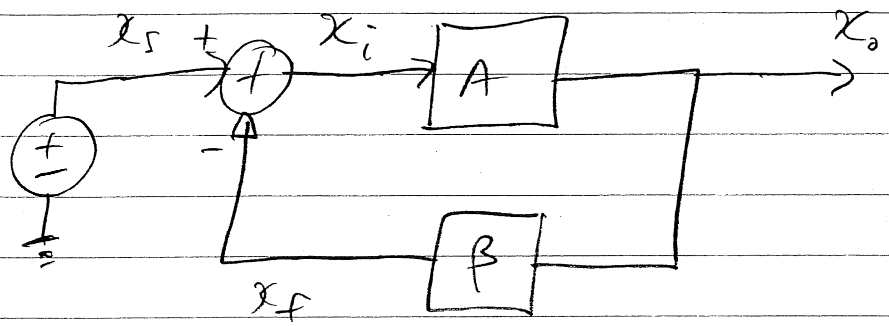
4 BASIC FEEDBACK STRUCTURES



4 BASIC TYPES DEPENDING ON TYPES OF SIGNALS AT x_s, x_f, x_i + x_o

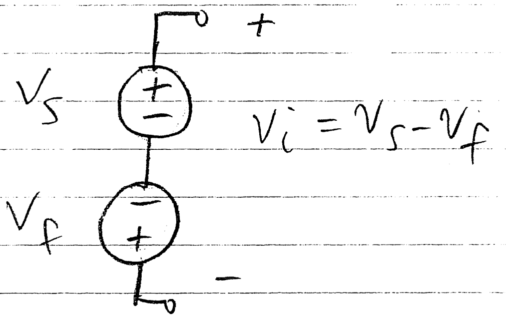
x_s, x_f, x_i	x_o	TYPE (INPUT/OUTPUT)
VOLTAGE	VOLTAGE	SERIES-SHUNT
CURRENT	VOLTAGE	SHUNT-SHUNT
CURRENT	CURRENT	SHUNT-SERIES
VOLTAGE	CURRENT	SERIES-SERIES

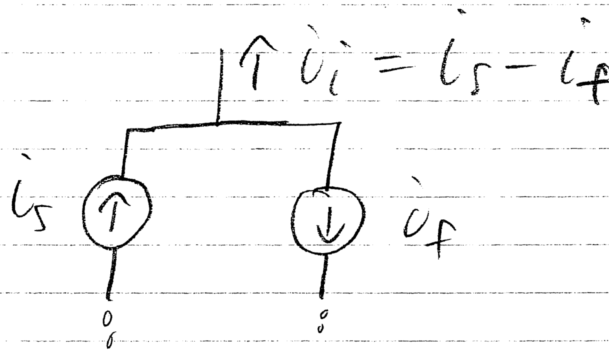
SO SERIES-SHUNT MEANS OUTPUT IS A VOLTAGE AND IS <u>SAMPLED</u> WITH A <u>SHUNT</u> NETWORK WHILE INPUT IS ALSO A VOLTAGE AND THE SUBTRACTION IS DONE WITH A <u>SERIES</u> NETWORK.

WHY THE TERMINOLOGY ⇒ SERIES / SHUNT?

INPUT SUMMATION

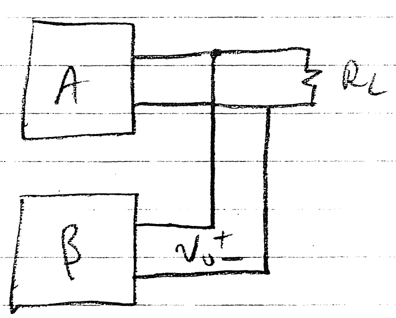
VOLTAGES ARE ADDED BY PUTTING THEM IN SERIES WHILE CURRENTS ARE ADDED BY PUTTING THEM IN PARALLEL (SHUNT)

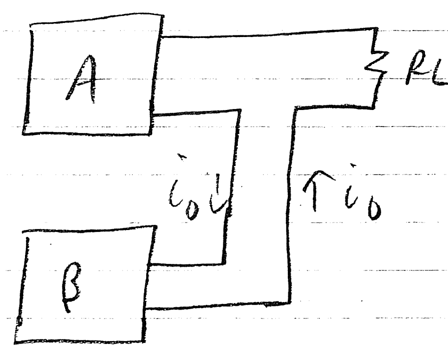




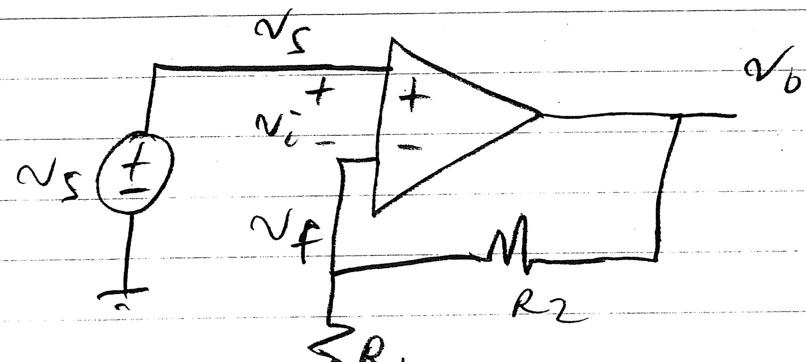
OUTPUT SAMPLING

VOLTAGES ARE SAMPLED BY A PARALLEL (SHUNT) CONNECTION WHILE CURRENTS ARE SAMPLED BY A SERIES CONNECTION





SERIES-SHUNT EXAMPLES



$v_i = v_s - v_f$

NEG FEEDBACK CHECK

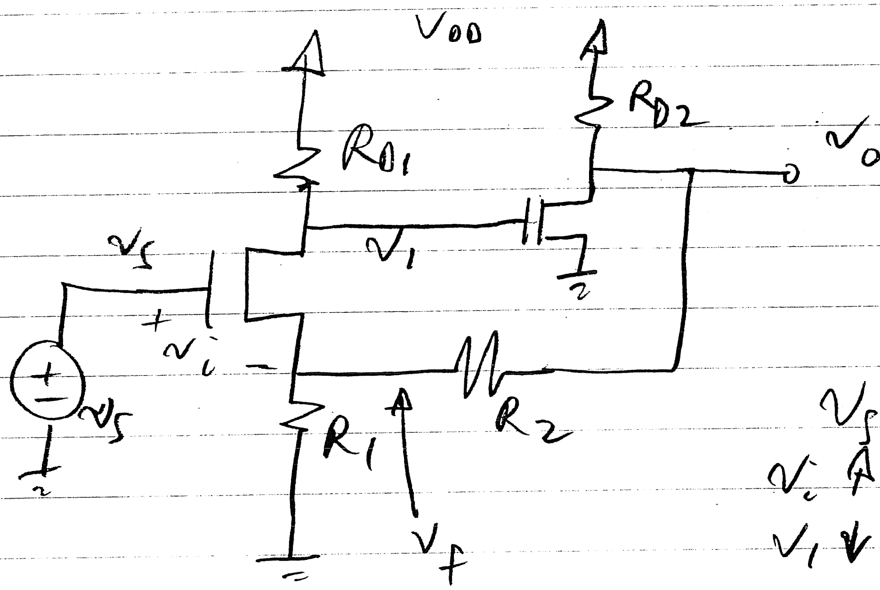
$v_s \uparrow \Rightarrow v_i \uparrow$

$v_i \uparrow \Rightarrow v_o \uparrow$

$v_o \uparrow \Rightarrow v_f \uparrow$

$v_f \uparrow \Rightarrow \underline{v_i \downarrow}$ ✓

OPPOSITE OF ORIGINAL v_i CHANGE



$v_i = v_s - v_f$

NEG FEEDBACK CHECK

$v_s \uparrow \Rightarrow v_i \uparrow$

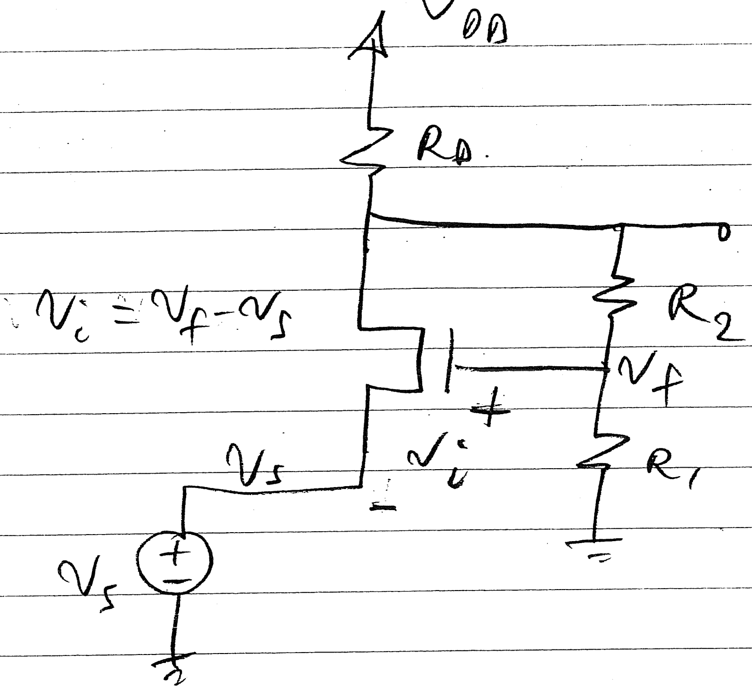
$v_i \uparrow \Rightarrow v_1 \downarrow$

$v_1 \downarrow \Rightarrow v_o \uparrow$

$v_o \uparrow \Rightarrow v_f \uparrow$

$v_f \uparrow \Rightarrow \underline{v_i \downarrow}$ ✓

FF3



NEG FEEDBACK CHECK

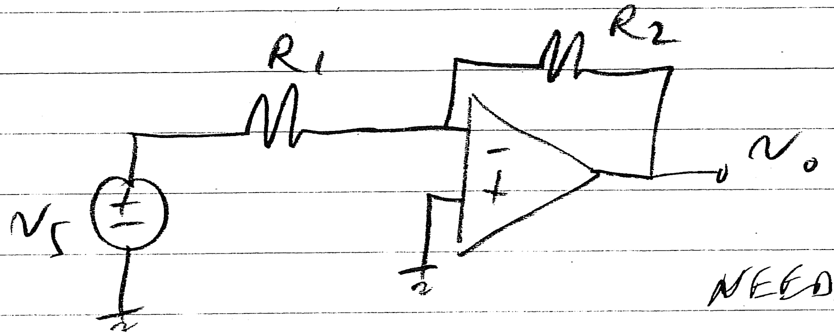
$v_s \uparrow \Rightarrow v_i \downarrow$

$v_i \downarrow \Rightarrow v_o \uparrow$

$v_o \uparrow \Rightarrow v_f \uparrow$

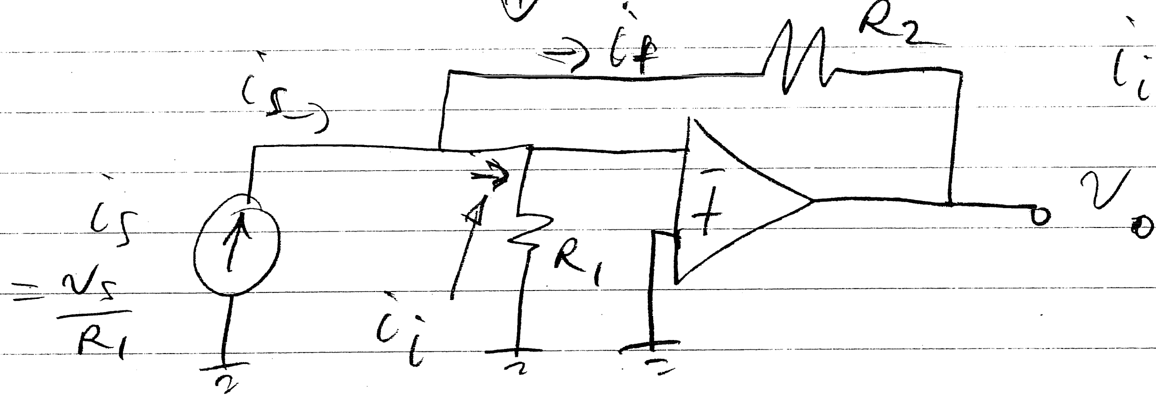
$v_o \uparrow \Rightarrow v_i \uparrow$ ✓ OPPOSITE OF ORIGINAL v_i CHANGE

SHUNT - SHUNT EXAMPLES



NEEDS MODIFICATION

⇓



$i_i = i_s - i_f$

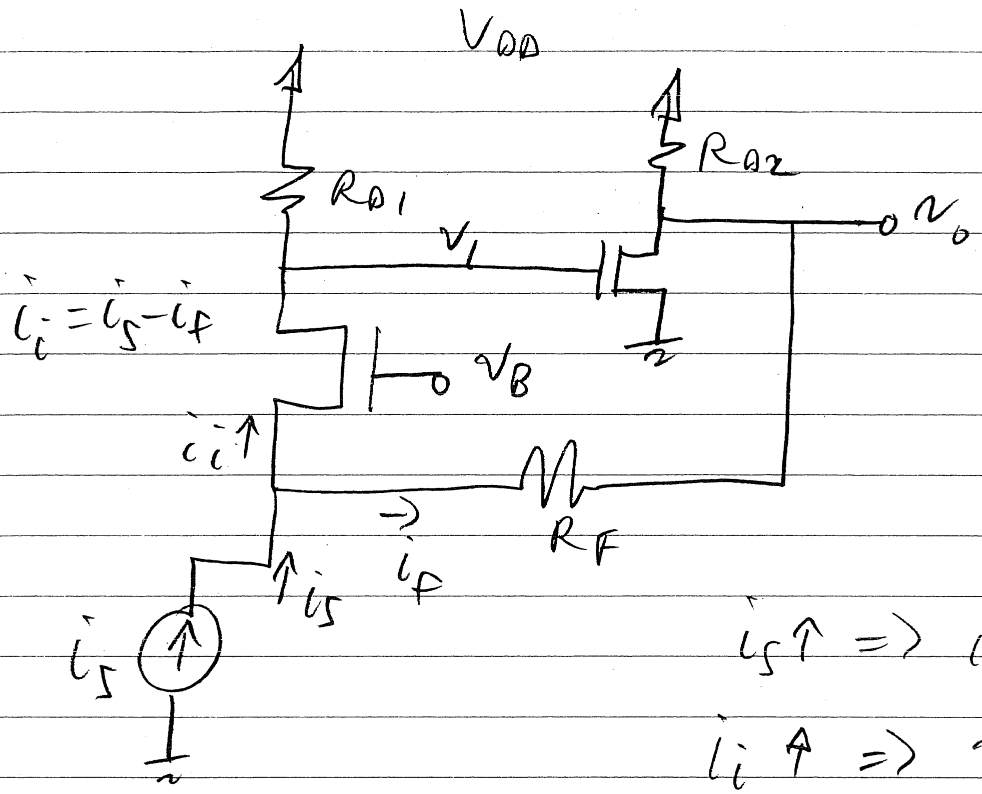
$i_s \uparrow \Rightarrow i_i \uparrow$

$i_i \uparrow \Rightarrow v_o \downarrow$ (SINCE $v_- \uparrow$ DUE TO $i_i \downarrow$ $v_o = A(v_+ - v_-)$)

$v_o \downarrow \Rightarrow i_f \uparrow$

$i_f \uparrow \Rightarrow i_i \downarrow$ ✓

FF5



$i_s \uparrow \Rightarrow i_i \uparrow$

$i_i \uparrow \Rightarrow v_1 \uparrow$

$v_1 \uparrow \Rightarrow v_o \downarrow$

$v_o \downarrow \Rightarrow i_f \uparrow$

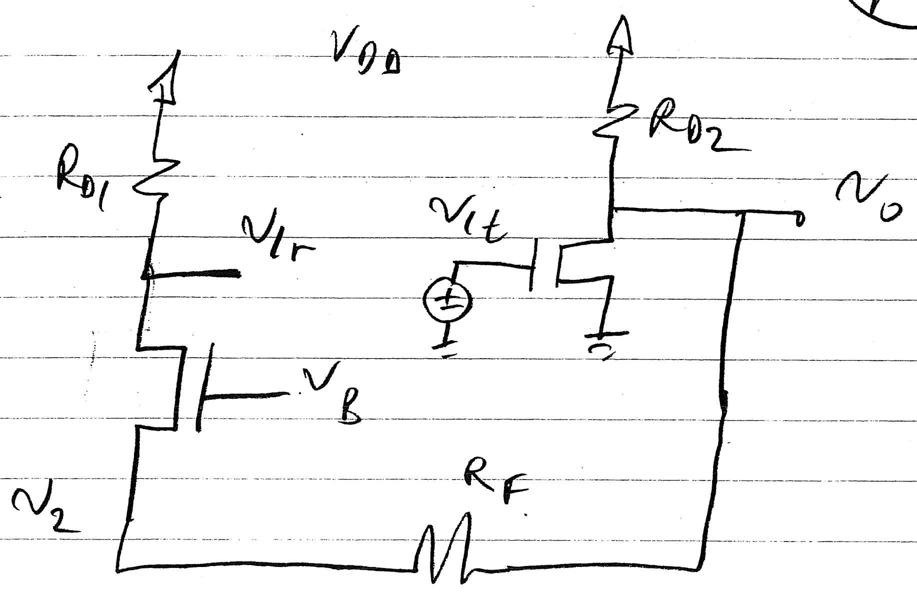
$i_f \uparrow \Rightarrow \underline{i_i \downarrow}$ ✓

A BIT MORE DIFFICULT TO SEE NEG FEEDBACK HERE. EASIER TO LOOK <u>AROUND</u> LOOP AT v_1 WITH $i_s = 0$ (OPEN)

BREAK LOOP AT $\underline{\underline{v_1}}$

INSERT TEST VOLTAGE v_{1t} + FIND <u>RETURN</u> SIGNAL v_{1r}

IF $v_{1t} \uparrow$ THEN $v_{1r} \downarrow$



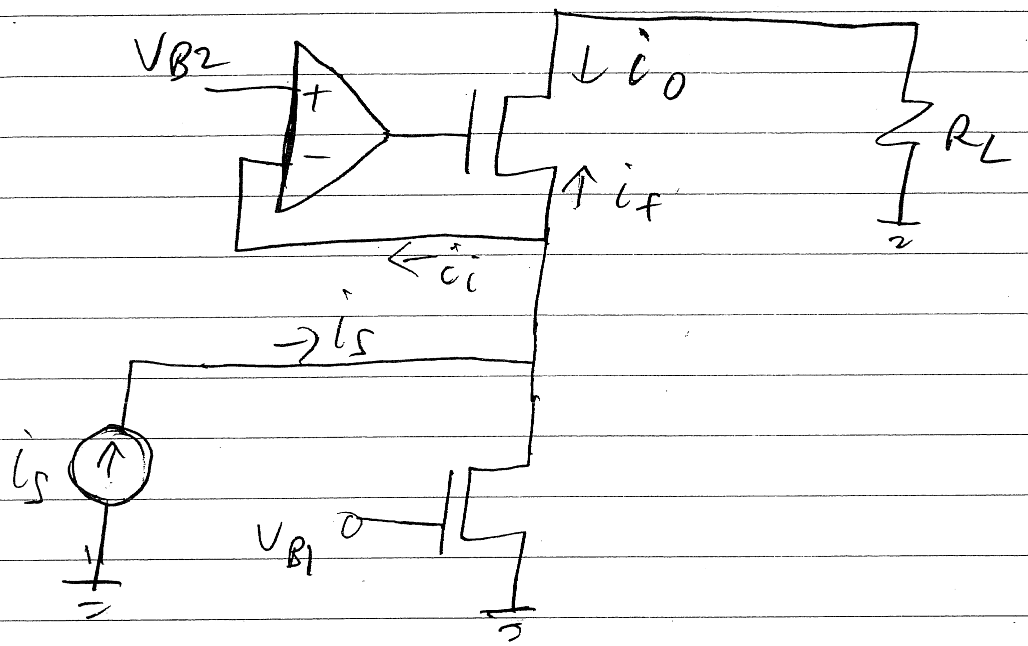
$v_{1t} \uparrow \Rightarrow v_o \downarrow$

$v_o \downarrow \Rightarrow v_2 \downarrow$

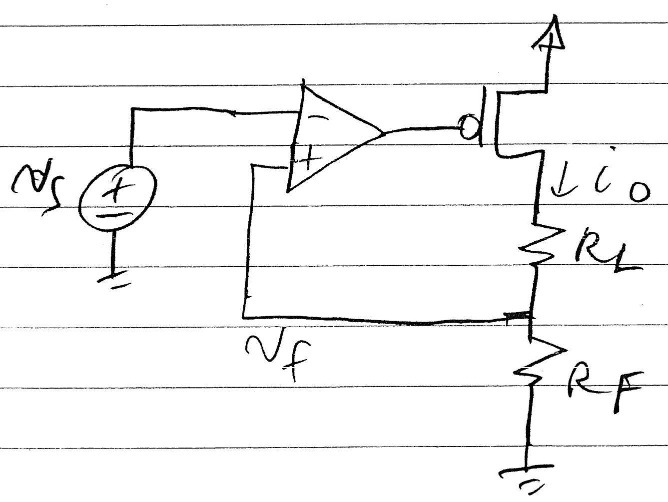
$v_2 \downarrow \Rightarrow v_{1r} \downarrow$ ✓

OPPOSITE OF v_{1t}

SHUNT-SERIES EXAMPLE



SERIES-SERIES EXAMPLE



- IN GENERAL, TYPE OF FEEDBACK IS DETERMINED BY WHERE INPUT IS APPLIED AND WHAT IS CONSIDERED TO BE THE OUTPUT.

- THIS MAKES 4 FEEDBACK APPROACH DIFFICULT TO USE & PRONE TO ERRORS

- WE SHALL DEVIATE FROM TEXTBOOK HERE AND USE THE
 LOOP GAIN ANALYSIS APPROACH

- IT IS DESCRIBED IN THE 5'TH EDITION OF "ANALYSIS AND DESIGN OF ANALOG INTEGRATED CIRCUITS" BY GRAY/HURST/LEWIS/MEYER, 2009

- ANOTHER ISSUE WITH 4 FEEDBACK APPROACH IS THAT $A\beta$ DEPENDS ON INPUT APPLIED + OUTPUT TAKEN ESPECIALLY WHEN β IS NOT UNIDIRECTIONAL

- THE LOOP GAIN IS UNCHANGED

 IN THE RETURN-RATIO APPROACH

- LOOP GAIN DETERMINES STABILITY OF A CIRCUIT.